

METHOD AND APPARATUS FOR PURIFYING POLLUTED SOIL, AND
APPARATUS FOR EMITTING CHLORINE-CONTAINING GAS AND
APPARATUS FOR DECOMPOSING POLLUTED GAS USING THE SAME

5 BACKGROUND OF THE INVENTION

Field of the Invention

The present invention relates to a method and an apparatus for purifying polluted soil and to an apparatus for emitting a chlorine-containing gas and an apparatus for decomposing a polluted gas using the same.

Related Background Art

With the development of industrial technology in recent years, the use of organochlorine compounds (for example, chlorinated ethylene and chlorinated methane) has become enormous, and the disposal of such compounds has become a serious problem. In addition, there have arisen serious environmental problems such as soil and groundwater pollutions with the used organochlorine compounds as pollutants. Thus efforts have been made so as to solve such problems.

To be concrete, one well-known example of the methods in common use of treating such pollutions is to dig up the soil and subject the same to heat treatment so as to separate hazardous pollutants therefrom, as disclosed in, for example, Japanese Patent Application Laid-Open No. 4-215708. Another well-known method in

current use is to expose the soil having organochlorine compounds mixed therein to microwave and subject the same to dielectric heating so as to remove the organochlorine compounds (Japanese Patent Application Laid-Open No. 8-164376).

In addition, it is known that chlorinated aliphatic hydrocarbons such as trichloroethylene and tetrachloroethylene are subjected to aerobic or anaerobic decomposition by microorganisms, and attempts have been made to decompose the chlorinated aliphatic hydrocarbons and purify the soil utilizing such a process.

On the other hand, as for the treatment other than the treatment for polluted soil, there are disclosed in Japanese Patent Application Laid-Open No. 54-66376 an electrolysis vessel for performing electrolysis using as an electrolysis solution a halide aqueous solution consisting of NaCl or NaBr and an apparatus including the above electrolysis vessel for removing an offensive odor by, first, aerating the cathode-side liquid in the electrolysis vessel with the gas as an odor source and, then, aerating the anode-side liquid in the electrolysis vessel with the gas used for the above aeration. However, with this apparatus, it is necessary to go through the processes of: aerating the cathode-side liquid in the electrolysis with a gas as an odor source; recovering the gas from the cathode-

side liquid; and aerating the anode-side liquid in the electrolysis vessel with the recovered gas. Therefore, the treatment of a gas as an odor source may not always be performed in a stable manner.

5 In Japanese Patent Publication No. 53-17816, there is disclosed a method of treating an organic waste fluid by dissolving aluminum chloride or iron chloride therein and electrolyzing the chloride while exposing the same to ultraviolet light. The above patent
10 publication states that the organic matter in a waste fluid can be decomposed with the active species of oxygen produced by the action of ultraviolet light on the chlorite which is produced from the chloride subjected to electrolysis.

15 However, even with the treatment method disclosed in the above patent publication, the treatment may not always be performed in a stable manner because of the changes in chloride concentration of the waste fluid.

20 It is also known that functional water obtained by electrolyzing water, for example, acid water has a bactericidal effect (Japanese Patent Application Laid-Open No. 1-180293) and a cleaning effect on contaminants on semiconductor wafers (Japanese Patent Application Laid-Open No. 7-51675).

25 These four patent publications, however, disclose nothing related to purification of the polluted soil.

SUMMARY OF THE INVENTION

In light of the facts that most technologies in current use of removing pollutants from the soil require further detoxification treatment as well as 5 relatively complicated apparatus for decomposing the pollutants, the present inventors concluded that providing a method and an apparatus for treating the polluted soil in a simple, stable and environment-friendly manner would enable the decrease in industrial 10 waste, which is inevitably produced with the industrial progress, as well as the decrease in the pollution due to the above industrial waste more easily, and hence, would largely contribute to the fields associated with 15 the polluted soil treatment.

Accordingly, the object of the present invention 15 is to provide a method of purifying polluted soil in a simple, efficient and stable manner and an apparatus for use in performing the above method, and in addition, an apparatus for emitting chlorine-containing 20 gas which is applicable to the purification of the polluted soil and an apparatus for decomposing polluted gas using the above chlorine-containing gas emitting apparatus.

The method of purifying the polluted soil 25 according to the present invention is as follows.

The method of purifying polluted soil which contains a pollutant according to the present invention

is characterized in that it includes the steps of:
heating the polluted soil to make a soil emit the
pollutant and bringing the emitted pollutant into
contact with functional water under light irradiation
5 to decompose the pollutant.

Another aspect of the method of purifying polluted
soil according to the present invention is
characterized in that it includes the steps of: heating
the polluted soil to make the soil emit a gas
10 containing the pollutant; passing a gas through
functional water to generate a gas containing chlorine;
mixing the pollutant-containing gas and the chlorine-
containing gas to form a gaseous mixture; and
irradiating the gaseous mixture with light to decompose
15 the pollutant.

The method of purifying polluted soil according to
the present invention embraces the following aspects.

Preferably the above heating is conducted using a
heater.

20 Preferably the step of the above heating includes
the step of mixing the polluted soil with an inorganic
compound which reacts exothermically with water.

Preferably rolling processing is conducted after
mixing the polluted soil with an inorganic compound.

25 Preferably stirring processing is conducted after
mixing the polluted soil with an inorganic compound.

Preferably the inorganic compound is at least one

selected from the group consisting of quick lime, magnesium oxide, barium oxide, strontium oxide, sodium oxide, potassium oxide, and anhydrides of calcium sulfate and magnesium sulfate, respectively.

5 Preferably the water content of the polluted soil is 10 to 30% by weight.

Preferably the functional water is water produced by electrolysis of water containing an electrolyte.

10 Preferably the functional water is acid functional water produced in the vicinity of anode by the electrolysis of the water containing an electrolyte.

Preferably the electrolyte is at least one selected from the group consisting of sodium chloride and potassium chloride.

15 Preferably the functional water is an aqueous solution containing hypochlorous acid.

Preferably the functional water containing hypochlorous acid is a hypochlorite aqueous solution.

20 Preferably the hypochlorite is at least one selected from the group consisting of sodium hypochlorite and potassium hypochlorite.

Preferably the functional water further contains an inorganic acid or an organic acid.

25 Preferably the inorganic acid or an organic acid is at least one selected from the group consisting of hydrochloric acid, hydrofluoric acid, oxalic acid, sulfuric acid, phosphoric acid, boric acid, acetic

acid, formic acid, malic acid and citric acid.

Preferably the functional water has a hydrogen ion concentration (pH value) of 1 to 4, an oxidation-reduction potential (working electrode: platinum electrode, reference electrode: silver-silver chloride electrode) of 800 to 1500 mV, and a chlorine concentration of 5 to 150 mg/l.

Preferably the functional water has a hydrogen ion concentration (pH value) of 4 to 10, an oxidation-reduction potential (working electrode: platinum electrode, reference electrode: silver-silver chloride electrode) of 300 to 1100 mV, and a chlorine concentration of 2 to 100 mg/l.

Preferably the light comprises a light whose wavelength is in the range of 300 to 500 nm.

Preferably the pollutant is a halogenated aliphatic hydrocarbon.

Preferably the halogenated aliphatic hydrocarbon is an aliphatic hydrocarbon compound having at least one selected from the group consisting of chlorine substituent and fluorine substituent.

Preferably the halogenated aliphatic hydrocarbon is at least one selected from the group consisting of trichloroethylene, 1,1,1-trichloroethane, tetrachloroethylene, cis-1,2-dichloroethylene, chloroform and dichloromethane.

Preferably the method further includes the step

of allowing an adsorption material to adsorb the pollutant.

Preferably the chlorine concentration of the gaseous mixture is in the range of 5 ppm to 1000 ppm.

5 Preferably the chlorine concentration of the gaseous mixture is in the range of 20 ppm to 500 ppm.

Preferably the gas passed through the functional water is the gas containing the pollutants extracted from the polluted soil.

10 The apparatus for purifying polluted soil which contains a pollutant according to the present invention is as follows.

The apparatus for purifying the polluted soil is characterized in that it includes a means for heating the polluted soil to make the soil emit the pollutant; a means for bringing the emitted pollutant into contact with functional water, and a means for irradiating the functional water with light.

Another aspect of the apparatus for purifying polluted soil according to the present invention is characterized in that it includes: a gas-emitting means for heating the polluted soil to make the soil emit a gas containing the pollutant; a chlorine-containing gas generating means for generating a gas containing chlorine by passing a gas through functional water; a mixing means for mixing the pollutant-containing gas and the chlorine-containing gas so as to form a gaseous

mixture; and a light irradiation means for irradiating the gaseous mixture with light.

The apparatus for purifying polluted soil according to the present invention embraces the 5 following aspects.

Preferably the heating is conducted using a heater.

Preferably the heating is conducted by mixing the polluted soil with an inorganic compound which reacts 10 exothermically with water.

Preferably the functional water is water produced by electrolysis of water containing an electrolyte.

Preferably the functional water is an aqueous solution containing hypochlorous acid.

15 Preferably the functional water has a hydrogen ion concentration (pH value) of 1 to 4, an oxidation-reduction potential (working electrode: platinum electrode, reference electrode: silver-silver chloride electrode) of 800 to 1500 mV, and a chlorine concentration of 5 to 150 mg/l.

20 Preferably the functional water has a hydrogen ion concentration (pH value) of 4 to 10, oxidation-reduction potential (working electrode: platinum electrode, reference electrode: silver-silver chloride electrode) of 300 to 1100 mV, and a chlorine concentration of 2 to 100 mg/l.

Preferably the light in the means for irradiating

the functional water with the light comprises a light whose wavelength is in the range of 300 to 500 nm.

Preferably the means for heating the polluted soil is a rotary kiln.

5 Preferably the chlorine concentration of the gaseous mixture is in the range of 5 ppm to 1000 ppm.

Preferably the chlorine concentration of the gaseous mixture is in the range of 20 ppm to 500 ppm.

10 Preferably the gas which is passed through the functional water is the gas containing the pollutant extracted from the polluted soil.

The present invention also embraces an apparatus for emitting a chlorine-containing gas.

15 The apparatus for generating a chlorine-containing gas according to the present invention is characterized in that it comprises a containing means for containing functional water; a functional water-supplying means for supplying the functional water to the above containing means; a first gas-supplying means for 20 supplying a gas through the functional water to generate a gas containing chlorine derived from the functional water; a second gas-supplying means for supplying the chlorine-containing gas to another containing means; and a concentration-measuring means 25 for measuring the concentration of the chlorine-containing gas; the functional water-supplying means, the first gas-supplying means, the second gas-supplying

means and the concentration-measuring means being connected to the containing means, respectively.

The apparatus for generating a chlorine-containing gas according to the present invention embraces the 5 following aspects.

The gas pass through the functional water does not react with the functional water. A great number of bubbles are created in the functional water by passing of the gas therethrough. The first gas-supplying means 10 can be controlled depending on the concentration of the chlorine-containing gas measured by the concentration-measuring means. And the functional water-supplying means can be controlled depending on the concentration of the chlorine-containing gas measured by the 15 concentration-measuring means.

Further, the present invention embraces an apparatus for decomposing a polluted gas.

The apparatus for decomposing a polluted gas according to the present invention is characterized in 20 that it comprises the apparatus for generating a chlorine-containing gas according to the present invention; a gas-containing means for containing a plurality of gases including a chlorine-containing gas supplied by the second gas-supplying means of the apparatus for generating a chlorine-containing gas; a 25 polluted gas-supplying means for supplying a polluted gas to the gas-containing means; and a light

irradiating means for irradiating the gases contained in the gas-containing means with light; the polluted gas-supplying means being connected to the gas-containing means.

5 The apparatus for decomposing a polluted gas according to the present invention embraces the following aspects.

10 The apparatus for decomposing a polluted gas according to the present invention can be constructed in such a manner that the the second gas-supplying means is connected to the gas-containing means

15 The apparatus for decomposing a polluted gas according to the present invention can be constructed in such a manner that a concentration-measuring means is arranged in the gas-containing means.

20 The apparatus for decomposing a polluted gas according to the present invention can be constructed in such a manner that the concentration of the chlorine-containing gas supplied by the second gas-supplying means or that of the polluted gas supplied by the polluted gas-supplying means is measured by the concentration-measuring means arranged in the gas-containing means.

25 The apparatus for decomposing a polluted gas according to the present invention can be constructed in such a manner that at least one of the concentration of the chlorine-containing gas supplied by the second

gas-supplying means, the irradiation intensity of the light irradiating means and the flow rate of the polluted gas supplied by the polluted gas-supplying means is controlled depending on the measured values of 5 the concentration-measuring means arranged in the gas-containing means.

The apparatus for decomposing a polluted gas according to the present invention can be constructed in such a manner that at least one of the flow rate of 10 the chlorine-containing gas supplied by the second gas-supplying means, the irradiation time of the light irradiating means and the flow rate of the polluted gas supplied by the polluted gas-supplying means is controlled depending on the measured values of the 15 concentration-measuring means arranged in the gas-containing means.

The apparatus for decomposing a polluted gas according to the present invention can be constructed in such a manner that the polluted gas-supplying means 20 is connected to the polluted soil-containing means for containing the polluted soil and can supply the polluted gas emitted from the polluted soil to the gas-containing means.

The apparatus for decomposing a polluted gas according to the present invention can be constructed 25 in such a manner that the polluted soil-containing means is provided with a heating means.

The apparatus for decomposing a polluted gas according to the present invention can be constructed in such a manner that the polluted soil-containing means is provided with a stirring means for stirring 5 the polluted soil contained therein.

The apparatus for decomposing a polluted gas according to the present invention can be constructed in such a manner that the polluted soil-containing means is provided with a concentration-measuring means 10 for measuring the concentration of a gas emitted from the polluted soil contained therein.

The apparatus for decomposing a polluted gas according to the present invention can be constructed in such a manner that the heating means or the stirring 15 means is controlled depending on the measured values of the concentration-measuring means for measuring the concentration of the gas emitted from the polluted soil.

According to the method and apparatus for 20 purifying polluted soil of the present invention, the decomposition of halogenated aliphatic hydrocarbon compounds, as pollutants, contained in the soil can be achieved thoroughly even at low costs, and hence, the purification of the soil. This is far different from 25 the methods and apparatus in current use in which halogenated aliphatic hydrocarbon compounds, as pollutants, are just transferred from the soil to the

media such as activated carbon.

Further, according to the apparatus for emitting a chlorine-containing gas of the present invention, a chlorine-containing gas can be emitted in a 5 controllable and stable manner. And according to the apparatus for decomposing a polluted gas of the present invention, which is constructed in such a manner as to arrange the above apparatus for emitting a chlorine-containing gas therein, a polluted gas can be 10 decomposed in a controllable and stable manner.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a schematic view showing one form of apparatus for purifying polluted soil embodying the 15 present invention;

FIG. 2 is a schematic view showing another form of apparatus for purifying polluted soil embodying the present invention;

FIG. 3 is a schematic view showing still another 20 form of apparatus for purifying polluted soil embodying the present invention;

FIG. 4 is a schematic view showing another form of apparatus for purifying polluted soil embodying the present invention;

25 FIG. 5 is a schematic view showing another form of apparatus for purifying polluted soil embodying the present invention;

FIG. 6 is a schematic view showing still another form of apparatus for purifying polluted soil embodying the present invention;

5 FIG. 7 is a schematic view showing another form of apparatus for purifying polluted soil embodying the present invention;

FIG. 8 is a schematic view showing another form of apparatus for purifying polluted soil embodying the present invention; and

10 FIG. 9 is a schematic view showing another form of apparatus for purifying polluted soil embodying the present invention.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

15 The present invention is described in detail.

The method for purifying polluted soil of the present invention is characterized in that it comprises the steps of heating the polluted soil to make the soil emit the pollutant, and bringing functional water, 20 which is capable of decomposing the pollutant in the presence of light, into contact with the emitted pollutant under light irradiation.

Another embodiment of the method for purifying polluted soil of the present invention is characterized 25 in that it comprises the steps of heating the polluted soil to make the soil emit a gas containing the pollutant, passing a gas through functional water to

generate a chlorine-containing gas, mixing the pollutant-containing gas with the chlorine-containing gas to form a gaseous mixture, and irradiating the gaseous mixture with light to decompose the pollutant.

5 The apparatus of the present invention for purifying polluted soil is provided, which comprises a means for heating the polluted soil to make the soil emit the pollutant, a means for bringing the emitted pollutant into contact with functional water, and a 10 means for irradiating the functional water with light.

15 Another embodiment of the apparatus of the present invention for purifying polluted soil is provided, which comprises a means for heating the polluted soil to make the soil emit a gas containing the pollutant, a means for generating the chlorine-containing gas by 20 passing a gas through functional water, a means for mixing the pollutant-containing gas with the chlorine-containing gas to form a gaseous mixture, and a means for irradiating the gaseous mixture with light.

25 In the method for purifying polluted soil and apparatus for purifying polluted soil of the present invention, it is preferable to heat the polluted soil by heater or by mixing an inorganic compound exothermically reacting with water to the soil.

30 The method for purifying polluted soil and apparatus for purifying polluted soil of the present invention broadly fall into two general categories: one

bringing functional water into contact with the pollutant under light irradiation, and the other irradiating, with light, the mixture of the gas polluted with the pollutant emitted from the soil by 5 heating the soil and chlorine-containing gas generated by passing the gas through functional water.

These two types of embodiments have the common features: the polluted soil is placed in a given closed space, where it is heated to emit the gaseous 10 pollutant.

In the type of embodiment with the functional water brought into contact with the pollutant while being irradiated with light, the gaseous pollutant emitted is sent to a reaction tank, where it is 15 brought into contact with the functional water. When irradiated with light, the functional group decomposes the pollutant dissolved therein by its decomposition function. The method for bringing the gaseous pollutant into contact with the functional water is not 20 limited, but it is preferable to secure a sufficient area for the gas/liquid contact. For example, it is preferable, when the gaseous pollutant is directly passed through the functional water, to keep the gas bubbles as small as possible. The functional group can 25 be also efficiently brought into contact with the gaseous pollutant, when it is finely divided by, e.g., spraying, or dropped onto, e.g., a plurality of

baffles.

On the other hand, in the type of embodiment where the mixture of the gas polluted with the pollutant and chlorine-containing gas evolved by passing the gas

5 through functional water is irradiated with light, the mixture of the gaseous pollutant and chlorine-containing gas evolved by passing a gas through the functional water is irradiated with light to decompose the pollutant.

10 In both types of embodiments, the pollutant adsorbed by soil is eventually emitted, to purify the polluted soil and, at the same time, the pollutant from the soil is decomposed, to complete the purification process.

15 FIG. 1 outlines one embodiment of the apparatus of the present invention for purifying polluted soil. It purifies soil polluted with a halogenated aliphatic hydrocarbon, e.g., organic chlorine compound, by releasing the compound from the soil and decomposing it. It is composed of the heating tank 2 which contains the polluted soil 1, functional water reaction tank 3 in which the functional water is brought into contact with the pollutant emitted, while being irradiated with light, and light emitting means 4, which emits light with which the functional water is irradiated. The heating tank 2 is designed in such a way to be supplied with the soil 1 polluted with, e.g.,

an organic chlorine compound, and is provided with the heating means 5 which can heat the polluted soil 1.

The apparatus of the above structure for purifying polluted soil places the soil 1 polluted with a halogenated aliphatic hydrocarbon compound, e.g., organic chlorine compound, at a given position in the heating tank 2, and heats the polluted soil 1 by the heating means 5, to emit the pollutant 1 and thereby to purify the polluted soil 1. This step may be referred to as the heating step. Then, the pollutant-containing gas is directed into the functional water reaction tank 3 by the pump 8, where the gas is passed through the functional water. The functional water reaction tank 3 is equipped with a functional water supply device (not shown), and the pipe 9 and pump 10 by which the functional water is supplied. The functional water is irradiate with light emitted from the light emitting means 4, to decompose the pollutant in the functional water. This step may be referred to as the purification/decomposition step. The used functional water for the treatment is discharged via the discharge pipe 6. The purified gas is discharged via the discharge pipe 7. The intake pipe 11 serves as the passage for air flowing into the tank 2 from the outside while the pump 8 is working. The stirring means 12 stirs the polluted soil 1. The apparatus may be further equipped with means for passing the gas

discharged via the pipe 7 over an adsorbent, e.g., activated carbon, to adsorb the undecomposed pollutant. Moreover, it may be so structured to concentrate the gas discharged from the heating step by adsorbing it on 5 an adsorbent, e.g., activated carbon, and to direct the gas emitted from the adsorbent to the functional water reaction tank 3.

Another embodiment of the apparatus for purifying the polluted soil is described by referring to FIG. 4. 10 The apparatus shown in FIG. 4 is of a type in which the mixture of the gas polluted with the pollutant emitted out of the heated soil and chlorine-containing gas evolved by passing the gas through functional water (This operation is also referred to as "aerating 15 functional water with the gas", hereinafter.) is irradiated with light, unlike the one shown in FIG. 1 in which the functional water is brought into contact with the pollutant while being irradiated with light.

Each member of the apparatus shown in FIG. 4 is 20 marked with the same number as the corresponding one in FIG. 1, when they have the same function. The apparatus shown in FIG. 4 is composed of the heating tank 2 which contains the polluted soil 1, functional water aeration tank 14 which aerates the functional 25 water to evolve the chlorine-containing gas, treatment tank 13 in which the pollutant-containing gas from the heating tank 2 is mixed with the chlorine-containing

gas evolved in the functional water aeration tank 14, and light emitting means 4, which emits light with which the mixed gas is irradiated.

The apparatus shown in FIG. 4 mainly differs from 5 the one shown in FIG. 1 in that the pollutant is directly decomposed not by the functional water by itself but by the chlorine-containing gas evolved by aeration of the functional water and that the chlorine-containing gas is supplied to the treatment tank 13 10 where it is mixed with the pollutant-containing gas.

The apparatus shown in FIG. 4 places the soil 1 polluted with a halogenated aliphatic hydrocarbon compound, e.g., organic chlorine compound, at a given position in the heating tank 2, and heats the polluted 15 soil 1 by the heating means 5, to emit the pollutant 1 and thereby to purify the polluted soil 1. The pollutant-containing gas is directed into the treatment tank 13 by the pump 8, and, at the same time, the gas is passed through the functional water to evolve the 20 chlorine-containing gas, which is directed into the treatment tank 13. The functional water aeration tank is equipped with a functional water supply device (not shown), and the pipe 9 and pump 10 by which the functional water is supplied. The functional water is 25 aerated by the pump 15 as the means for supplying the gas into the functional water. It is preferable to form a number of bubbles in the functional water, in

order to efficiently evolve the chlorine-containing gas.

The gaseous mixture in the treatment tank 13 is irradiate with light emitted from the light emitting means 4, to decompose the pollutant in the mixture. This step may be referred to as the purification/decomposition step. The used functional water for the treatment is discharged out of the functional water aeration tank 14 via the discharge pipe 6. The purified gas is discharged via the discharge pipe 7. The intake pipe 11 serves as the passage for air flowing into the tank 2 from the outside while the pump 8 is working. The stirring means 12 stirs the polluted soil 1. The apparatus may be further equipped with means for passing the gas discharged via the pipe 7 over an adsorbent, e.g., activated carbon, to adsorb the undecomposed pollutant. Moreover, it may be so structured to concentrate the gas discharged from the heating step by adsorbing it on an adsorbent, e.g., activated carbon, and to direct the gas emitted from the adsorbent to the treatment tank 13.

The decomposition process is not fully understood. It is however considered that electrolysis of water containing an electrolyte, e.g., sodium chloride, generates the functional water or the like in the vicinity of the anode, which contains hypochlorous acid

or hypochlorite to make the water acidic and increase chlorine existing ratio. The chlorine radicals or the like are possibly excited, when the solution is irradiated with light, to accelerate decomposition of
5 the pollutant.

Passing air through the functional water transfers chlorine from the water into the vapor phase, and chlorine is mixed with the pollutant also in the vapor phase. The chlorine radicals or the like are possibly
10 excited, when the gaseous mixture is irradiated with light, to accelerate decomposition of the pollutant. It is considered that the decomposition proceeds mainly in the vapor phase rather than in the liquid phase.

In the heating step, a heater may be replaced by
15 an inorganic compound exothermically reacting with water, which is added to the polluted soil. The heat generated by the exothermic reaction evaporates the volatile organic chlorine compound from the soil. This brings about the advantage of massively treating the
20 polluted soil at a cost lower than that required for heating the soil by the heater.

An indirect heating type unit, e.g., rotary kiln, may be used for heating the polluted soil to emit the pollutant therefrom. It contains the polluted soil in
25 a rotating tubular body, heats the soil being stirred in the rotating tubular body from the outside to above boiling point of the pollutant, and evaporated the

pollutant into carrier air supplied from the outside to emit the pollutants out of the unit. It well matches the constitutional requirements of the present invention.

5 Next, the apparatus for generating a chlorine-containing gas of the present invention and the apparatus for decomposing a polluted gas also of the present invention, incorporating the former apparatus, are described. The apparatus for generating a

10 chlorine-containing gas of the present invention is comprised of a containing means for containing functional water; a functional water-supplying means for supplying the functional water to the containing means; a first gas-supplying means for supplying a gas through the functional water to generate a gas containing chlorine derived from the functional water; a second gas-supplying means for supplying the chlorine-containing gas to another containing means; and a concentration-measuring means for measuring the

15 concentration of the chlorine-containing gas; the functional water-supplying means, the first gas-supplying means, the second gas-supplying means and the concentration-measuring means being connected to the containing means, respectively.

20 The apparatus for decomposing a polluted gas of the present invention is comprised of a gas-containing means for containing a plurality of gases including a

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chlorine-containing gas supplied by the second gas-supplying means of the apparatus for generating a chlorine-containing gas; a polluted gas-supplying means for supplying a polluted gas to the gas-containing means; a light irradiating means for irradiating the gases contained in the gas-containing means with light, the polluted gas-supplying means being connected to the gas-containing means; and the apparatus for generating a chlorine-containing gas of the present invention.

10 The chlorine-containing gas evolving unit and polluted gas decomposing unit of the present invention are described by referring to FIG. 6. Each member of the unit shown in FIG. 6 is marked with the same number as the corresponding one in FIG. 1 or 4, when they have 15 the same function.

FIG. 6 schematically illustrates one embodiment of the polluted gas decomposing unit of the present invention, in which the chlorine-containing gas evolving unit of the present invention is used.

20 Referring to FIG. 6, the chlorine-containing gas evolving unit of the present invention is composed of the functional water aeration tank 14 (functional water containing means), pipe 9 and pump 10 (functional water supplying means), pump 15 for passing the gas through 25 the functional water (gas supplying means), pump 31 for supplying the chlorine-containing gas to the gas containing means (gas supplying means), and sensor 16

for measuring concentration of the chlorine-containing gas in the functional water aeration tank 14 (concentration measuring means). The polluted gas decomposing unit of the present invention comprises the 5 above chlorine-containing gas evolving unit, treatment tank 13 (gas-containing means for treating two or more types of gases), pump 8 for supplying the polluted gas containing the pollutant to the treatment tank 13 (polluted material supplying means), and light emitting 10 means 4 which emits light onto the gas contained in the treatment tank 13. The unit of this embodiment is further provided with the sensor 16 for measuring concentration of the gas in the treatment tank 13 or functional water aeration tank 14, and controller 17 15 which transmits the control signal 63 to the pump 10 as the functional water supplying means and/or pump 15 as the means for supplying the gas to the functional water, based on the gas concentration information signals 61 and/or 62 from the sensor 16 provided in the 20 functional water aeration tank 14 and/or treatment tank 13. This system controls flow rate of the functional water to be supplied to the functional water aeration tank 14 and/or of the gas aerating the functional water, and hence controls concentration and flow rate 25 of the chlorine-containing gas contained in the aeration tank 14 at optimal levels.

The above chlorine-containing gas evolving unit of

the present invention can therefore stably evolve chlorine-containing gas whose concentration is controlled at a desired level. The polluted gas decomposing unit of the present invention, comprising 5 the above chlorine-containing gas evolving unit, can stably supply the chlorine-containing gas of desired concentration from the chlorine-containing gas evolving unit to the treatment tank 13, and, at the same time, efficiently decompose the pollutant gas in the 10 treatment tank 13, because concentration of the gas in the treatment tank 13 is measured by the sensor 16 and feedbacked based on concentration information of the gaseous mixture of the gas polluted with the pollutant and chlorine-containing gas in the treatment tank 13.

15 Next, the apparatus of the present invention for purifying polluted soil, comprising the polluted gas decomposing unit of the present invention, is described by referring to FIG. 7. The apparatus shown in FIG. 7 comprises the polluted gas decomposing unit shown in 20 FIG. 6, and the unit extracting the gas containing the pollutant emitted out of the polluted soil by heating, which is composed of the heating tank 2 which contains the polluted soil 1, heating means 5 provided in the heating tank 2, and means 12 for stirring the polluted 25 soil 1, wherein the heating tank 2 is connected to the pump 8 (FIG. 6) to send the polluted gas containing the pollutant to the treatment tank 13. The heating tank 2

is provided with the sensor 16 for measuring concentration of the gas in the tank 2, the concentration information signal of the gas in the tank 2 being transmitted to the controller 17. Therefore, 5 the apparatus for purifying polluted soil is provided with the sensor in the unit for supplying the gas containing the pollutant, in addition to the sensors provided in the functional water aeration tank 14 (non-electrolysis tank) and treatment tank 13, to measure 10 concentration of the gas in each tank and thereby optimally control each unit that constitutes the apparatus in accordance with the gas concentration. This design helps purify the polluted soil highly 15 efficiently and stably.

15 Control of the apparatus shown in FIG. 7 is described. The following information items are inputted in the controller 17, where the number in the parenthesis after each information item or control name corresponds to the one shown in FIG. 7.

20 Functional water aeration tank 14: Chlorine gas concentration (71)

Heating tank 2: Pollutant concentration (gas), temperature, or stirring speed (each 72)

25 Treatment tank 13: Pollutant concentration, chlorine gas concentration (each 73)

The following devices can be controlled, based on one of the above input information items:

Pump 10: Control of flow rate of the functional water
(74)

Pump 15: Control of flow rate of the gas for aeration
(74)

5 Heating means 5: Control for heating temperature

Stirring means 12: Control of stirring speed

Pump 8: Control of flow rate of the polluted gas (75)

Light emitting means 4: Control of emitted light
intensity

10 The concrete control examples are described below:

1. Control of the functional water aeration tank 14
(Concentration of chlorine gas)

(1) When chlorine gas concentration decreases to below
the desired level: Increase flow rate at the pump 10
15 and/or decrease flow rate at pump 15

(2) When chlorine gas concentration increases to above
the desired level: Decrease flow rate at the pump 10
and/or increase flow rate at pump 15

20 The chlorine gas concentration may be controlled
mainly by the flow rate at the pump 10, when
disturbances of the overall flow balances are to be
minimized.

2. Control of the heating tank 2 (Concentration of the
pollutant, temperature or stirring speed)

25 (1) When pollutant concentration decreases to below the
desired level: Increase temperature at the heating
means 5, and/or increase speed of rotation at the

stirring means 12, and/or decrease flow rate at the pump 8

(2) When pollutant concentration increases to above the desired level: Decrease temperature at the heating means 5, and/or decrease speed of rotation at the stirring means 12, and/or increase flow rate at the pump 8.

The pollutant concentration may be controlled mainly by temperature at the heating means 5, and/or speed of rotation at the stirring means 12, when disturbances of the overall flow balances are to be minimized. It is preferable to adjust temperature at the heating means and speed of rotation at the stirring means slowly, even under the normal conditions, because pollutant concentration changes slowly.

3. Control of the treatment tank 13 (Pollutant or chlorine gas concentration)

(1) When the pollutant remains: Increase chlorine concentration, and/or increase emitted light intensity, and/or decrease pollutant concentration, and/or decrease flow rate of the pollutant, and/or decrease the overall flow rate (or increase residence time)

(2) When chlorine remains: Decrease chlorine concentration, and/or increase pollutant concentration, and/or increase flow rate of the pollutant, and/or increase the overall flow rate (or decrease residence time)

In the actual control of the apparatus, 1. control of the functional water aeration tank 14, 2. control of the heating tank 2, and 3. control of the treatment tank 13 may be combined one another.

5 Next, the apparatus shown in FIG. 8 is described. It is the apparatus shown in FIG. 7 in which the functional water aeration tank 14 is combined with the treatment tank 13, and this portion is highlighted in FIG. 8. It has the functional water reaction tank 3, 10 serving the functions of the functional water aeration tank 14 and treatment tank 13 shown in FIG. 7, and the sensor 16 provided in the reaction tank 3. In this apparatus, the gas for aerating the functional water is supplied via the pump 9 to the functional water 15 reaction tank 3, and the functional water is aerated by the gas. Thus, this apparatus evolves the chlorine-containing gas in the functional water reaction tank 3, and mixes this gas with the pollutant-containing gas supplied via the pump 8. In this state, the gaseous 20 mixture is irradiated with light from the light emitting means 4, to decompose the pollutant. The apparatus can be controlled by the aid of sensors 16 in a manner similar to the one described above.

Next, the apparatus shown in FIG. 9 is described. 25 It is the apparatus shown in FIG. 9 which further incorporates the unit for supplying the pollutant-containing gas, composed of the heating tank 2,

stirring means 12 and sensors 16 in addition to the apparatus shown in FIG. 8. It has the functional water reaction tank 3, which is a combination of the functional water aeration tank 14 and treatment tank 13, shown in FIG. 7. It can be controlled in the same manner as the one shown in FIG. 7, except that the gaseous mixture in the functional water reaction tank 3 is irradiated with light.

The present invention is described in more detail.
10 (Polluted soil to be treated)

The type of polluted soil to be treated by the present invention is not limited. The pollutants to be removed are preferably those decomposable with a functional water and light. These include halogenated 15 aliphatic hydrocarbon compounds, which contain at least one of chlorine and fluorine. The present invention is particularly suitable for removing organic chlorine compounds. These compounds include trichloroethylene, 1,1,1-trichloroethane, tetrachloroethylene, cis-1,2- dichloroethylene, chloroform, and dichloromethane. 20 Those having a boiling point of 60 to 120°C at normal pressure are suitable, when an inorganic compound exothermically reacting water is used as the heat source. These include, for example, 1,1,1-trichloroethane, trichloroethylene, tetrachloroethylene, chloroform and ethane dichloride.

(Heating means)

The heating means for the present invention is not limited. Heat may be supplied from an electrical heater, or generated by an exothermic reaction.

(When an electrical heater is used)

5 Any heater may be used to heat the polluted soil in the heating tank. When a microwave oscillator for the normal microwave oven for domestic purposes (2,450 MHZ, 1.2 kW) is used, surface temperature of, e.g., 120°C can sufficiently evaporate the pollutant from the 10 soil. The system is a dry system, using no steam for heating, and shows good energy-saving effect and is installed at a relatively low cost.

(When an inorganic compound exothermically reacting with water is used)

15 The suitable inorganic compounds exothermically reacting with water include oxides of alkali metal and alkali-earth metals, and sulfates of alkali-earth metals, e.g., quick lime, magnesium oxide, barium oxide, strontium oxide, sodium oxide, potassium oxide, 20 anhydrides of calcium sulfate and magnesium sulfate. Of these, quick lime is more preferable for its safety, cost and heat generating efficiency. Commercially available industrial quick lime may be used, and the one having a purity of 85% or more as CaO is preferable 25 for the present invention to fully exhibit its effect. The inorganic compound suitable for the present invention is normally powdery or granular, the latter

being more preferable for its workability when it is to be mixed with the soil.

When mixed with the soil polluted with a halogenated aliphatic hydrocarbon compound, the 5 inorganic compound reacts with water in the soil to generate heat, thereby evaporating and releasing the halogenated aliphatic hydrocarbon compound.

The present invention exhibits its effect especially notably, when the polluted soil to be 10 treated contains water at 10 to 30 wt.% (which is a normal range of water content). It is therefore preferable, when water is present at below 10 wt.% in the soil, that water is sprayed onto, and mixed with, the soil before treatment, to increase its water 15 content to at least 10 wt.%.

The method to mix the inorganic compound with the soil is not limited. The inorganic compound, e.g., quick lime, may be sprayed onto the soil, and physically mixed therewith at the site, or it may be 20 placed in soil to form a sandwich structure. Thus, it may be mixed with the soil evenly or unevenly, the former being more preferable for the effect for removing the halogenated aliphatic hydrocarbon compound. The polluted soil may be collected, and 25 mixed evenly in another place or in a container, depending on circumstances.

It is preferable to adjust the soil in such a way

to keep its temperature at 15°C or higher, preferably 30°C or higher, while it is mixed with the inorganic compound, although varying depending on desired extent for mixing and quantity and water content of the 5 polluted soil, in order to reduce time and increase efficiency for removing the halogenated aliphatic hydrocarbon compound. For the polluted soil containing water at 10 to 30 wt.%, for example, quantity of quick lime of 0.01 to 0.5 times of the water quantity in the 10 polluted soil to be treated, preferably 0.05 to 0.3 times, is sufficient to attain the purpose.

It is preferable to subject the polluted soil mixed with the inorganic compound roll processing (compression using physical means). This will ensure 15 closer contact between the inorganic compound and water in the polluted soil, and accelerate heat accumulation during the initial stage, leading to reduced time for heating the polluted soil, increased efficiency for insulating the soil, and hence increased efficiency for 20 removing the halogenated aliphatic hydrocarbon compound. The method for increasing pressure is not limited. For example, the polluted soil may be physically compressed by a roller.

Time required for removing the halogenated 25 aliphatic hydrocarbon compound can be reduced, and hence removal efficiency can be increased, by mixing the organic compound and then well stirring the

polluted soil when its temperature reaches the peak or
nearby level. In particular, even when the polluted
soil is solidified to some extent by compression, a
simple stirring procedure divides the polluted soil
5 particles to be more fine to sufficiently bring about
the above effect, because incorporation of the
inorganic compound decreases water content of the soil
to make the soil less viscous and more fluid.

10 The halogenated aliphatic hydrocarbon compound
thus emitted is decomposed, when irradiated with light
while in contact with the functional water, to purify
the polluted soil.

15 The pollutant emitted is also decomposed and made
harmless.

15 (Functional water generator and functional water)
The functional water to be used in the functional
water reaction tank includes, e.g., water having a
hydrogen ion concentration (pH value) of 1 to 4, redox
potential of 800 to 1,500 mV with platinum as the
20 working electrode and silver/silver oxide as the
reference electrode, and chlorine concentration of 5 to
150 mg/l.

Such functional water may be prepared by
electrolysis of water dissolving an electrolyte (e.g.,
25 sodium chloride or potassium chloride) in a water tank
provided with a pair of electrodes. It is produced in
the vicinity of the anode. Preferable electrolyte

content is 20 to 2,000 mg/l, in case of sodium chloride. Disposition of a membrane between a pair of electrodes can produce the functional water capable for decomposing the organic compound more efficiently,
5 because it prevents the acidic functional water generated in the vicinity of the anode from being mixed with alkaline water generated in the vicinity of the cathode. The suitable membrane includes an ion-exchanging membrane.

10 The functional water may be produced by a commercial generator of strongly acidic electrolyzed water (e.g., Asahi Glass Engineering's Oasis BiohalfTM, and Amano's Model FW-200TM). The functional water produced by a generator having no membrane may be also
15 used for decomposition of the organic compound, when it has a redox potential of 300 to 1,100 mV, chlorine concentration of 2 to 100 mg/l and pH of 4 to 10.

Electrolysis is not the sole method for preparing the functional water. Water which undergoes no
20 electrolysis can decompose an organic chlorine compound almost as effectively as the one prepared by electrolysis, when incorporated with various reagents, e.g., 0.001 to 0.1 mol/l of hydrochloric acid, 0.005 to 0.02 mol/l of sodium chloride and 0.0001 to 0.01 mol/l
25 of sodium hypochlorite. The functional water having a pH level of 4 or more can be also prepared without depending on electrolysis by incorporating various

reagents, e.g., 0.001 to 0.1 mol/l of hydrochloric acid, 0.001 to 0.1 mol/l of sodium hydroxide and 0.0001 to 0.01 mol/l of sodium hypochlorite, or only sodium hypochlorite at 0.0001 to 0.01 mol/l. The functional water having pH of 4.0 or less and effective chlorine content of 2 mg/l or more may be also prepared with hydrochloric acid and sodium hypochlorite.

5 Hydrochloric acid may be replaced by another inorganic acid (e.g., hydrofluoric, sulfuric, phosphoric or boric acid) or organic acid (e.g., acetic, formic, malic, citric or oxalic acid). In addition, the functional water may be prepared using, e.g., $\text{N}_3\text{C}_3\text{O}_3\text{NaCl}_2$ (e.g., Clean Chemical's Kinosan 21XTM), which is commercially available as the agent for 10 producing a weakly acidic, aqueous powder. The functional water incorporated with these additives can decompose an organic chlorine compound to varying extent, when irradiated with light, as described in one of Examples. The raw water for the functional water 15 may be service water, river water, seawater, or the like. The raw water normally has pH of 6 to 8 and contains chlorine at 1 mg/l at the highest, and naturally shows no capacity for decomposing an organic chlorine compound.

20 Any type of the functional water described above shows high capacity for decomposing an organic chlorine compound, when irradiated with light, and is useful for

the present invention.

(Chlorine gas concentration, and means for
evolving chlorine gas)

It is possible to evolve a chlorine-containing gas
5 necessary for decomposition from the functional water.
The chlorine-containing gas may be evolved by passing a
gas through the functional water for the present
invention, or by various other methods. For example,
10 the chlorine-containing gas may be efficiently evolved
by, e.g., bringing a gas (e.g., air) into contact with
the functional water finely divided by, e.g., spraying,
or by bringing the functional water into contact with
air or the like while being dropped onto a plurality of
15 baffles. The gas to be passed through, or brought into
contact with, the functional water is preferably not
reactive with the functional water, e.g., inert gas,
nitrogen gas, or air. A mixture of the gas to be
decomposed and chlorine gas may be obtained by passing
the pollutant-containing gas instead of air or the like
20 through the functional water. In this case, a chlorine
gas of relatively high concentration can be obtained.

The mixture of the gas to be decomposed and
chlorine gas is preferably adjusted to have a chlorine
concentration of 5 to 1000 ppm, although varying
25 depending on concentration of the gas to be treated.
In particular, the gas can be decomposed very
efficiently when the concentration is 20 to 500 ppm,

more preferably 80 to 300 ppm.

(Light emitting means)

The light emitting means for the present invention preferably emits light having a wavelength of 300 to 5 500 nm. The pollutant can be decomposed practically sufficiently, when the functional aqueous solution, gas which has passed through the functional water and pollutant to be decomposed are irradiated with light having an intensity of several hundreds $\mu\text{W}/\text{cm}^2$ 10 (wavelength: 300 to 400 nm) for a light source having a peak at a wavelength of around 360 nm.

The reaction tank may be made of glass, plastic or the like, because the light emitted is completely free of ultraviolet component harmful to a human body, 15 having a wavelength of around 250 nm or less.

The light sources useful for the present invention include those emitting natural light such as solar ray, or artificial light, e.g., mercury lamp, black light or colored fluorescent lamp.

20 One of the embodiments of the present invention passes a gas through the functional water to evolve the chlorine-containing gas necessary for decomposing the pollutant. The section for passing the gas through the functional water basically serves as the role for 25 supplying chlorine necessary for the decomposition. The vapor-phase reaction in the subsequent tank for the treatment and decomposition is mainly responsible for

the decomposition. Therefore, the ratio of the vapor phase section to the liquid phase section is an important parameter for decomposition capacity of the apparatus, when the evolution of chlorine and 5 decomposition of the pollutant are effected in the same vessel.

More concretely, increasing volume of the functional water increases quantity of chlorine to be supplied, but decreases volume of the vapor phase 10 section, thus decreasing the decomposition field. So is vice versa. Increasing volume of the vapor phase section increases volume of the reaction field, accelerating the decomposition, but decreases volume of the liquid phase section, decreasing chlorine to be 15 supplied. When the evolution of chlorine gas and decomposition (treatment) are effected in the same vessel, it is recommended that the liquid phase accounts for 5 to 30%, preferably 10 to 20%, of the treatment tank, although there are other parameters 20 (e.g., aeration speed and charge rate of chlorine-containing water) to be considered. When the above steps are effected in separate vessels, it is recommended to keep the tank for evolution of chlorine-containing air and tank for the decomposition in a 25 ratio of around 1:2 to 1:9 by volume.

(Means for passing gas through the functional water)

It is preferable to use a diffuser for passing a gas through the functional water, when the gas contains the pollutant and/or is used for aeration. The diffuser may be a normal one used for blowing a gas into a liquid, but is preferably selected from those which produce the bubbles of size having a sufficient surface areas for diffusing chlorine.

The diffuser is preferably made of a material which is not reactive with the pollutant and functional water component. Those useful for the present invention include porous diffuser plates of sintered glass, porous ceramics, sintered stainless steel (e.g., SUS316) and woven nets of stainless steel (e.g., SUS316) fibers, and spargers of glass and stainless steel (e.g., SUS316) pipes.

The present invention is described more concretely by Examples.

Example 1

Polluted soil was purified by the apparatus for purifying the polluted soil, shown in FIG. 1.

The polluted soil 1, polluted with organic chlorine compounds and the like, was charged into the heating tank 2 of stainless steel.

The pollutants and their contents are given below:

Trichloroethylene: 11.3 mg/kg

Tetrachloroethylene: 8.1 mg/kg

Dichloromethane: 2.3 mg/kg

1,1,1-trichloroethane: 8.3 mg/kg

An electrical heater (silicon rubber heater) was used as the heating means 5, to heat the polluted soil and emit the pollutant therefrom. The pollutant-
5 containing gas was charged into the functional water reaction tank 3, where it was passed through the functional water.

The functional water used in Example 1 was produced by a strong acid electrolyzed water generator
10 (Asahi Glass Engineering's Oasis Biohalf™ (ADE-61)). It had a pH level of 2.2, redox potential of 1,150 mV, residual chlorine concentration of 55 mg/l. The functional water in the reaction tank was irradiated with black light from the light emitting means 4
15 (Toshiba's FL20BLB™, 20W). The functional water reaction tank was a glass column, allowing no light having a wavelength of 300 nm or less to permeate therethrough.

The pollutant, discharged via the discharge pipe
20 7, were analyzed by gas chromatography (chromatograph: Shimadzu's GC-14B™ equipped with an FID detector, column: J&W's DB-624™). The concentrations of all the pollutant were below the detectable limit. The treated soil was immediately put in a 10 ml container
25 containing n-hexane, and stirred for 10 min. The hexane-layer was collected and analyzed by ECD chromatography. The concentrations of all the

pollutant were 0.01 mg/kg or less.

It is thus confirmed that the polluted soil was purified and the pollutants emitted were decomposed.

Example 2

5 Polluted soil was purified by the apparatus for purifying the polluted soil, shown in FIG. 2, where each member of the apparatus is marked with the same number as the corresponding one in FIG. 1, when they have the same function.

10 The polluted soil 1, polluted with organic chlorine compounds and the like, was charged into the heating tank 2 of stainless steel.

The pollutants and their contents are given below:

Trichloroethylene: 11.3 mg/kg

15 Tetrachloroethylene: 8.1 mg/kg

Dichloromethane: 2.3 mg/kg

1,1,1-trichloroethane: 8.3 mg/kg

An inorganic compound exothermically reacting with water was used as the heating means. More concretely, 20 a given quantity of quick lime (purity: 90% or more as CaO), crushed into particles of 5 mm as average size, was well mixed with the polluted soil 1 by the stirring means 12.

25 The heat generated by the exothermic reaction in the polluted soil 1 evaporated the pollutants. The exothermic reaction was continued for 24 hours with stirring, and the pollutant-containing gas was charged

into the functional water reaction tank 3 using the pump 8. The functional water reaction tank 3 and functional water contained therein were similar to those for Example 1.

5 The pollutant-containing gas was passed through the functional water in the same manner as in Example 1, and the functional water in the reaction tank 3 was irradiated with black light from the light emitting means 4. The pollutants, discharged via the discharge 10 pipe 7, were analyzed in the same manner as in Example 1. The concentrations of all the pollutants were below the detectable limit, and the treated soil was found to contain the pollutants all at 0.01 mg/kg or less. It is thus confirmed that the polluted soil was purified 15 and all pollutants emitted were decomposed.

Example 3

Polluted excavation soil 21, containing 10.3 mg/kg of trichloroethylene and 18.0 wt.% of water, was transferred into the vinyl house 22, shown in FIG. 3. 20 Temperature of the polluted soil was 11°C. Quick lime (CaO content: 90% or more) was evenly sprayed onto the polluted soil surface to 4 wt.%, based on the whole polluted soil, and stirred by a scoop for mixing. The mixture was immediately compressed by a roller, and 25 temperature rise was monitored. Stirring by a scoop was started when temperature reached to the attainable peak. Temperature of the mixture changed in a range

between 25 to 33°C, when it was stirred a couple of times. Concentration of trichloroethylene was decreased to 0.9 mg/kg in 10 hours. The mixture was again stirred in a similar manner for additional 10 5 hours. Its temperature changed in a range between 22 to 29°C, and concentration of trichloroethylene was further decreased to 0.01 mg/kg or less. At this stage, the polluted soil contained water at 12.7 wt.%. Stirring crushed the solidified soil into fine 10 particles of uniform size.

The polluted air in the vinyl house was transferred by the pump 28 to the functional water reaction/treatment unit 23, where the polluted air was passed through the functional water. Then, the inside 15 of the unit 23 was irradiated with black light emitted from the light emitting means 24. The functional water was prepared in the same manner as in Example 1.

The vapor-phase concentration of trichloroethylene emitted into the vinyl house changed in a range from 1 20 to 10 ppm during the polluted soil treatment period (approximately 20 hours), whereas its concentration at the outlet 27 of the functional water reaction/treatment unit was kept at 1 ppm or less.

Example 4

25 The test was conducted in the same manner as in Example 2, except that the functional water prepared by electrolysis was replaced by service water incorporated

with 0.006 mol/l of hydrochloric acid and 0.002 mol/l of sodium hypochlorite to have a pH level of 2.3, redox potential of 1,180 mV and chlorine concentration of 105 mg/l. The concentrations of all the pollutant,
5 discharged via the discharge pipe 7, were below the detectable limit, and the treated soil was found to contain the pollutants all at 0.01 mg/kg or less. It is thus confirmed that the polluted soil was purified and the pollutants emitted were decomposed.

10 Example 5

Polluted soil was purified by the apparatus for purifying the polluted soil, shown in FIG. 4.

15 The polluted soil 1, polluted with organic chlorine compounds and the like, was charged into the heating tank 2 of stainless steel.

The pollutants and their contents are given below:

Trichloroethylene: 12.0 mg/kg

Tetrachloroethylene: 8.7 mg/kg

Dichloromethane: 2.1 mg/kg

20 1,1,1-trichloroethane: 8.2 mg/kg

An electrical heater (silicon rubber heater) was used as the heating means 5, to heat the polluted soil and emit the pollutants therefrom. Air was sent via the pump 15 into the functional water aeration tank 14
25 to prepare the chlorine-containing air, which was sent into the treatment tank 13 together with the pollutant-containing air from the heating tank 2. The gaseous

mixture in the treatment tank 13 was irradiated with light from the light emitting means 4, to decompose the pollutants.

The functional water used in Example 5 was 5 produced by a strong acid electrolyzed water generator (Asahi Glass Engineering's Oasis Biohalf™ (ADE-61)). It had a pH level of 2.2, redox potential of 1,150 mV, residual chlorine concentration of 75 mg/l. The functional water in the treatment tank was irradiated 10 with black light from the light emitting means 4 (Toshiba's FL20BLB™, 20W). The treatment tank 13 was a glass column, allowing no light having a wavelength of 300 nm or less to permeate therethrough.

The chlorine-containing air, evolved in the 15 functional water aeration tank 14 of polypropylene, contained chlorine at 108 ppm (determined by Gastec's detector tube).

The pollutants, discharged via the discharge pipe 7, were analyzed in the same manner as in Example 1. 20 The concentrations of all the pollutant were below the detectable limit. The treated soil was also analyzed in the same manner as in Example 1. It was found to contain the pollutant all at 0.01 mg/kg or less.

It is thus confirmed that the polluted soil was 25 purified and the pollutants emitted were decomposed.

Example 6

Polluted soil was purified by the apparatus for

purifying the polluted soil, shown in FIG. 5. Each member of the apparatus shown in FIG. 5 is marked with the same number as the corresponding one in FIG. 1, when they have the same function.

5 The polluted soil 1, polluted with organic chlorine compounds and the like, was charged into the heating tank 2 of stainless steel.

The pollutants and their contents are given below:

Trichloroethylene: 12.0 mg/kg
10 Tetrachloroethylene: 8.7 mg/kg
Dichloromethane: 2.1 mg/kg
1,1,1-trichloroethane: 8.2 mg/kg

Heated air was supplied via the intake pipe 11 to the heating tank 2, to heat the polluted soil and emit 15 the pollutants therefrom. The pollutant-containing air was sent into the functional water reaction tank 3, where it was passed through the functional water.

In this example, the same conditions, e.g., apparatus configuration and functional water 20 properties, as for Example 1 were used, except that quantity of the functional water in the functional water reaction tank was reduced to one-eighth and only the vapor phase was irradiated with light.

The pollutant, discharged via the discharge pipe 25 7, was analyzed in the same manner as in Example 1. The concentrations of all the pollutants were below the detectable limit. The treated soil was also analyzed

in the same manner as in Example 1. It was found to contain the pollutants all at 0.01 mg/kg or less.

It is thus confirmed that the polluted soil was purified and the pollutants emitted were decomposed.

5 Example 7

Polluted soil was purified by the apparatus for purifying the polluted soil, shown in FIG. 8.

10 The polluted soil, polluted with organic chlorine compounds and the like, was charged into the heating tank of stainless steel (not shown in FIG. 8) in the same manner as in Example 1.

The pollutants and their contents are given below:

15 Trichloroethylene: 10.5 mg/kg
 Cis-dichloroethylene: 5.0 mg/kg
 1,1,1-trichloroethane: 7.5 mg/kg

20 An electrical heater (silicon rubber heater) was used as the heating means, to heat the polluted soil and emit the pollutants therefrom. The pollutant-containing gas was sent into the functional water reaction tank 3, where it was passed through the functional water.

25 In this example, the same conditions, e.g., apparatus configuration and functional water properties, as for Example 6 were used, except that pollutants and chlorine gas concentrations in the functional water reaction tank 3 were monitored, to investigate the optimum purification conditions.

In this example, the functional water reaction tank 3 was provided with a sample nozzle for the sensor 16 in FIG. 8, a gas chromatograph (Shimadzu's GC-14BTM equipped with an FID detector, column: J&W's DB-624TM) 5 or detector tube (Gastec's) which determined the pollutant component concentrations or chlorine gas concentration.

Table 1 gives the test conditions, the measured values inside the functional water reaction tank and 10 the concentrations of pollutants of the gas sampled at the discharge pipe 7 for each run. Unit of each flow rate is ml/min, corresponding to (: one liter) unit of the functional water reaction tank 3.

[Table 1]

15

Run No.	Flow rate of pollutant-containing gas (ml/min)	Flow rate of functional water (ml/min)	Pollutant gas concentration in the functional water reaction tank (ppm as trichloroethylene)	Chlorine gas concentration in the functional water reaction tank (ppm)	Pollutant gas concentration at the discharge pipe 7 (ppm as trichloroethylene)
1	300	2	not exceed 0.1	20 - 40	not exceed 0.1
2	600	2	not exceed 0.1	10 - 25	not exceed 0.1
3	900	2	not exceed 0.1	3 - 10	not exceed 0.1
4	900	1	not exceed 0.1	0 - 3	not exceed 0.1
5	900	0.5	1 - 2	0	0.1 - 1.0
6	900	3	not exceed 0.1	35 - 70	not exceed 0.1

20

As shown in Table 1, polluted soil can be 25 optimally treated by controlling flow rate of each stream without excess cost. In this Example, Run No. 4 is considered to provide the optimal conditions, under

which each pollutant concentration tended to decrease with time, causing surplus chlorine gas.

The treated soil was analyzed in the same manner as in Example 1. It was found to contain each of the 5 pollutants at 0.01 mg/kg or less.

It is thus confirmed that the polluted soil was purified and the pollutants emitted were decomposed.